

FOURIER OPTICS

I. THE DIFFRACTION INTEGRAL:

It may be fairly said that "it is well known" that plane waves are solutions of the homogeneous Helmholtz equation.¹ Thus, by a generalization of the Fourier theorem, we expect to be able to write a general solution for a given component of the (magnetic) vector potential in the form

$$\mathbf{A}(\vec{\mathbf{r}}, z) = \int \mathbf{A}(\vec{\mathbf{q}}, z) \exp[-j\vec{\mathbf{q}} \cdot \vec{\mathbf{r}}] \sqrt{k^2 - q_x^2 - q_y^2} dq_x dq_y dq_z \quad [\text{I-1}]$$

where the inclusion of the **Dirac delta function** insures that the Helmholtz equation is satisfied.² Executing the integration over q_z we obtain³

$$\begin{aligned} \mathbf{A}^\pm(\vec{\mathbf{r}}, z) = & \int \mathbf{A}^\pm(q_x, q_y, z) \exp[-j q_x x] \exp[-j q_y y] \\ & \times \exp[\mp j \sqrt{k^2 - q_x^2 - q_y^2} z] dq_x dq_y \end{aligned} \quad [\text{I-2}]$$

Evaluating this expression in the **paraxial approximation**, leads to the expression

¹ For the record the homogeneous Helmholtz equation is

$$\nabla^2 \vec{\mathbf{A}}(\vec{\mathbf{r}}, z) + \mu_0 \epsilon_0 \omega^2 \vec{\mathbf{A}}(\vec{\mathbf{r}}, z) = 0$$

² The Dirac delta function is defined as

$$\int_{x_0-a}^{x_0+b} f(x) \delta(x-x_0) dx = f(x_0)$$

³ It's a fussy point, but there are, of course two valid values of q_z -- viz. $\pm \sqrt{k^2 - q_x^2 - q_y^2}$. To remind ourselves of this slight complication, we include a \pm superscript on the vector potential and other variables to account for the possibility of fields propagating in either or both the positive (upper sign) and negative (lower sign) z -directions.

$$A^\pm(\vec{r}, z) = \exp[\mp j k z] \int \int A^\pm(q_x, q_y, z_0) \exp[-j q_x x] \exp[-j q_y y] \exp[\pm j \frac{q_x^2 + q_y^2}{2k} (z - z_0)] dq_x dq_y \quad [\text{I-3}]$$

If the vector potential is known over some particular plane, say the plane $z = z_0$, then

$$A^\pm(q_x, q_y, z_0) = \frac{1}{2} \int \int \exp[\pm j k z_0] \exp[\mp j q_x x] \exp[\mp j q_y y] A^\pm(x, y, z_0) \exp[j q_x x] \exp[j q_y y] dx dy \quad [\text{I-4}]$$

Therefore, the general solution in the paraxial approximation may be written

$$A^\pm(x, y, z) = \exp[\mp j k (z - z_0)] \int \int \exp[-j q_x x] \exp[-j q_y y] \exp[\pm j \frac{q_x^2 + q_y^2}{2k} (z - z_0)] \times \frac{1}{2} \int \int A^\pm(x', y', z_0) \exp[j q_x x'] \exp[j q_y y'] dx' dy' dq_x dq_y \quad [\text{I-5}]$$

Inverting the order of the integrations, we obtain

$$A^\pm(x, y, z) = \exp[\mp j k (z - z_0)] \frac{1}{2} \int \int \exp[-j q_x (x - x')] \exp[\pm j \frac{q_x^2}{2k} (z - z_0)] dq_x \times \exp[-j q_y (y - y')] \exp[\pm j \frac{q_y^2}{2k} (z - z_0)] dq_y A^\pm(x', y', z_0) dx' dy' \quad [\text{I-6}]$$

Finally, we write

$$A^\pm(x, y, z) = \exp[\mp j k (z - z_0)] \int \int A^\pm(x', y', z_0) \exp[\pm j \frac{q_x^2}{2k} (z - z_0)] \exp[\pm j \frac{q_y^2}{2k} (z - z_0)] dx' dy' \quad [\text{I-7a}]$$

where

$$h^\pm(x-x', z-z_0) = \frac{1}{2} \int_{-\infty}^{\infty} \exp[-j q_x (x-x')] \exp \pm j \frac{q_x^2}{2k} (z-z_0) dq_x \quad [\text{I-7b}]$$

Completing the square in the exponent by adding and subtracting a term $\frac{j k (x-x')^2}{2(z-z_0)}$

$$h^\pm(x-x', z-z_0) = \frac{1}{2} \int_{-\infty}^{\infty} \exp \mp \frac{j k (x-x')^2}{2(z-z_0)} \exp \pm \frac{j (z-z_0)}{2k} \left[\frac{k (x-x')^2}{(z-z_0)} \mp \frac{2 k q_x (x-x')}{(z-z_0)} + q_x^2 \right] dq_x \quad [\text{I-8}]$$

and using the standard form

$$\int_{-\infty}^{\infty} \exp[-a^2 u^2] du = \sqrt{\pi}/a \quad [\text{I-9}]$$

we obtain

$$A^\pm(x, y, z,) \pm \frac{1}{j(z-z_0)} \exp[\mp j k (z-z_0)] A^\pm(x', y', z_0,) \exp \mp \frac{j k [(x-x')^2 + (y-y')^2]}{2(z-z_0)} dx' dy' \quad [\text{I-10}]$$

which is the very famous Fresnel diffraction integral or paraxial integral equation. It can be shown that the *kernel* or *Green's function* of the diffraction integral -- i.e.

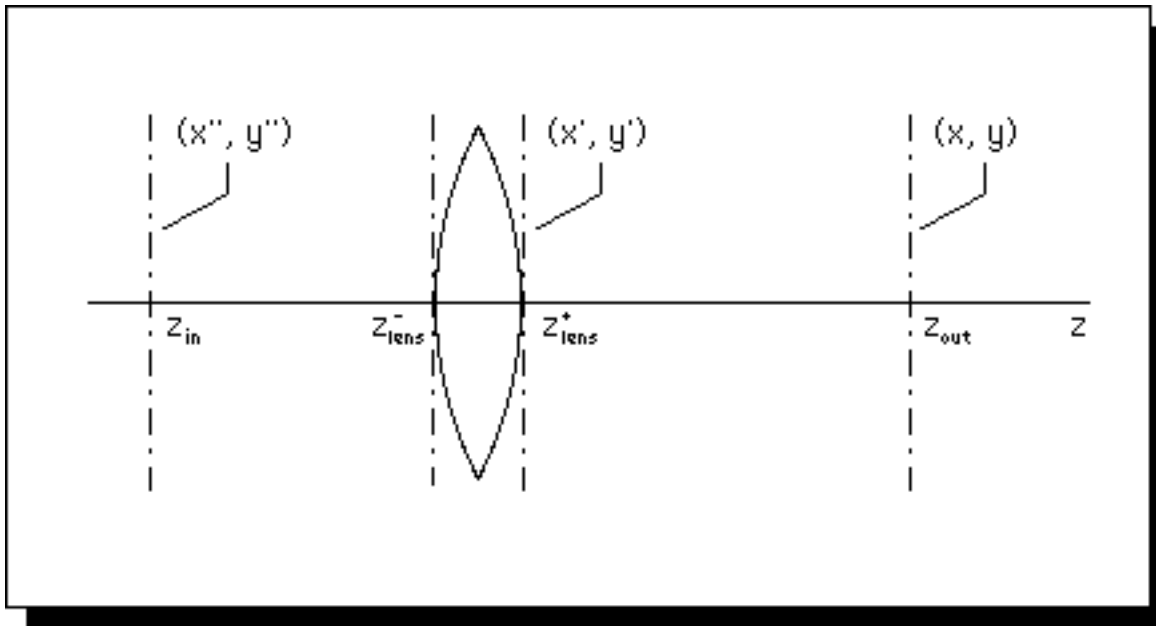
$$h^\pm(x-x', y-y'; z-z_0) \exp \mp \frac{j k [(x-x')^2 + (y-y')^2]}{2(z-z_0)} \quad [\text{I-11}]$$

-- is a solution of the paraxial wave equation. To recapitulate, the Fresnel diffraction integral may be expressed

$$A^\pm(x, y, z) \pm \frac{1}{j(z-z_0)} \exp[\mp jk(z-z_0)] \int \int A^\pm(x', y', z_0) h^\pm(x-x', y-y'; z-z_0) dx dy \quad [\text{I-12}]$$

II. OPTICAL SIGNAL PROCESSING:

In applying this result, let us first consider the simplest unit optical processor.



Optical Signal Processor

We find the field at $z = z_{out}$ in terms of the field at $z = z_{in}$ by successive iterations of the transform in Equation [I-12]. First, make the Fresnel transformation from $z = z_{lens}^+$ to $z = z_{out}$ ⁴

⁴ In what follows, we assume only fields propagating in the positive z-direction and thus may drop the fussy \pm superscript and factors included in earlier more complete expressions.

$$A(x, y, z_{out}) = \frac{1}{j(z_{out} - z_{lens})} \exp[-j k (z_{out} - z_{lens})] \int \int A(x', y', z_{lens}^+) h(x - x', y - y'; z_{out} - z_{lens}) dx' dy' \quad [\text{II-1}]$$

then, make the phase transformation across the thin lens from $z = z_{lens}^-$ to $z = z_{lens}^+$

$$A(x, y, z_{out}) = \frac{1}{j(z_{out} - z_{lens})} \exp[-j k (z_{out} - z_{lens})] \int \int A(x', y', z_{lens}^-) \exp[-j k n D - \frac{j k (x'^2 + y'^2)}{2f}] h(x - x', y - y'; z_{out} - z_{lens}) dx' dy' \quad [\text{II-2}]$$

and finally, once again make the Fresnel transformation from $z = z_{in}$ to $z = z_{lens}^-$

$$A(x, y, z_{out}) = \frac{1}{j(z_{out} - z_{lens})} \exp[-j k (nD + z_{out} - z_{lens})] \int \int \frac{1}{j(z_{lens}^- - z_{in})} \exp[-j k (z_{lens}^- - z_{in})] A(x', y', z_{in}) h(x - x', y - y'; z_{lens}^- - z_{in}) dx' dy' \quad [\text{II-3}]$$

$$\times \exp \frac{j k (x'^2 + y'^2)}{2f} h(x - x', y - y'; z_{out} - z_{lens}) dx' dy'$$

Inverting the order of the integrations and using the definition of kernel in Equation [I-11],

we obtain

$$A(x, y, z_{out}) = \frac{\exp[-j k (nD + z_{out} - z_{in})]}{j^2 (z_{out} - z_{lens})(z_{lens}^- - z_{in})} \exp \frac{j k (x^2 + y^2)}{2(z_{out} - z_{lens})} \int \int A(x', y', z_{in}) \exp \frac{j k (x'^2 + y'^2)}{2(z_{lens}^- - z_{in})} \times \mathbf{I}[x', y', (z_{lens}^- - z_{in}); x, y, (z_{out} - z_{lens})] dx' dy' \quad [\text{II-4}]$$

where

$$\begin{aligned}
 \mathbf{I} \left[x, y, (z_{lens} - z_{in}); x, y, (z_{out} - z_{lens}) \right] &= \exp \left[-\frac{j k}{2} \frac{1}{z_{out} - z_{lens}} + \frac{1}{z_{lens} - z_{in}} - \frac{1}{f} \right] (x^2 + y^2) \\
 &\times \exp \left[j k x \frac{x}{z_{out} - z_{lens}} + \frac{x}{z_{lens} - z_{in}} \right] \\
 &\times \exp \left[j k y \frac{y}{z_{out} - z_{lens}} + \frac{y}{z_{lens} - z_{in}} \right] dx dy
 \end{aligned} \tag{II-5}$$

If the thin lens is **infinite in extent** or, equivalently, if we neglect, for the moment, any effect of the finite size of the lens aperture, the result is fairly straight forward and we may write

$$\mathbf{I} \left[x, y, (z_{lens} - z_{in}); x, y, (z_{out} - z_{lens}) \right] = \mathbf{J} \left(\frac{x}{z_{out} - z_{lens}}, \frac{x}{z_{lens} - z_{in}} \right) \mathbf{J} \left(\frac{y}{z_{out} - z_{lens}}, \frac{y}{z_{lens} - z_{in}} \right) \tag{I-6}$$

where

$$\mathbf{J} \left(\frac{x}{z_{out} - z_{lens}}, \frac{x}{z_{lens} - z_{in}} \right) = \int_{-\infty}^{\infty} \exp \left[j \left(\frac{x^2}{z_{out} - z_{lens}} + \frac{x^2}{z_{lens} - z_{in}} \right) \right] dx \tag{I-7a}$$

$$\mathbf{J} \left(\frac{y}{z_{out} - z_{lens}}, \frac{y}{z_{lens} - z_{in}} \right) = \int_{-\infty}^{\infty} \exp \left[j \left(\frac{y^2}{z_{out} - z_{lens}} + \frac{y^2}{z_{lens} - z_{in}} \right) \right] dy \tag{I-7b}$$

$$-\frac{k}{2} \frac{1}{z_{out} - z_{lens}} + \frac{1}{z_{lens} - z_{in}} - \frac{1}{f} \tag{I-7c}$$

$$\frac{k}{z_{out} - z_{lens}} \frac{x}{z_{lens} - z_{in}} \quad \text{and} \quad \frac{k}{z_{out} - z_{lens}} \frac{y}{z_{lens} - z_{in}} \tag{I-7d}$$

By completing the square in the exponential, we see that

$$\begin{aligned} \mathbf{J}(a, b) &= \int_{-a}^{+a} \exp[j(a u^2 + b u)] du \\ &= \exp[-j b^2/4 a] \int_{-a}^{+a} \exp[j a (u + b/2 a)^2] du \end{aligned} \quad \text{[II-8]}$$

$$\begin{aligned} \mathbf{J}(a, b) &= \int_{-a}^{+a} \exp[j(a u^2 + b u)] du \\ &= \exp[-j b^2/4 a] \int_{-a}^{+a} \exp[j a (u + b/2 a)^2] du \end{aligned} \quad \text{[II-8]}$$

and so the standard form in Equation [I-9] yields

$$\mathbf{J}(a, b) = \begin{cases} (j/a)^{1/2} \exp[-j(b^2/4a)] & \text{for } a \neq 0 \\ 2(b) & \text{for } a = 0 \end{cases} \quad \text{[II-9]}$$

Consider, then, two important applications of this result:

1. The field in the image-plane -- *i.e.* $z = 0$, the condition for **imaging** in geometric optics.

$$\begin{aligned} \mathbf{I} &= \mathbf{I} \left[x, y, (z_{lens} - z_{in}); x, y, (z_{out} - z_{lens}) \right] \\ &= \frac{k x}{z_{out} - z_{lens}} + \frac{k x}{z_{lens} - z_{in}} = \frac{k y}{z_{out} - z_{lens}} + \frac{k y}{z_{lens} - z_{in}} \end{aligned} \quad \text{[II-10]}$$

and, thus,

$$A(x, y, z_{out}) = \frac{z_{lens} - z_{in}}{z_{out} - z_{lens}} \exp[-j k (n D + z_{out} - z_{in})] \exp \left[-\frac{j k (x^2 + y^2)(z_{out} - z_{in})}{2 (z_{out} - z_{lens})^2} \right] \times A \left(-\frac{z_{lens} - z_{in}}{z_{out} - z_{lens}} x, -\frac{z_{lens} - z_{in}}{z_{out} - z_{lens}} y, z_{in} \right) \quad [\text{II-11}]$$

or

$$|A(x, y, z_{out})| = \frac{z_{lens} - z_{in}}{z_{out} - z_{lens}} \left| A \left(-\frac{z_{lens} - z_{in}}{z_{out} - z_{lens}} x, -\frac{z_{lens} - z_{in}}{z_{out} - z_{lens}} y, z_{in} \right) \right| \quad [\text{II-12}]$$

2. The field in back focal-plane -- *i.e.* $z_{out} - z_{lens} = f$ so that

$$= -\frac{k}{2(z_{lens} - z_{in})}, \quad x = k \frac{x}{f} + \frac{x}{z_{lens} - z_{in}}, \quad \text{and} \quad y = k \frac{y}{f} + \frac{y}{z_{lens} - z_{in}}$$

and, thus,

$$J(x, y) = -\frac{j 2 (z_{lens} - z_{in})^{1/2}}{k} \exp \left[j \frac{k (z_{lens} - z_{in})}{2} \left(\frac{x}{f} + \frac{x}{z_{lens} - z_{in}} \right)^2 \right] \quad [\text{II-13a}]$$

$$J(x, y) = -\frac{j 2 (z_{lens} - z_{in})^{1/2}}{k} \exp \left[j \frac{k (z_{lens} - z_{in})}{2} \left(\frac{y}{f} + \frac{y}{z_{lens} - z_{in}} \right)^2 \right] \quad [\text{II-13a}]$$

$$A(x, y, z_{out}) = \frac{1}{j f} \exp[-j k (n D + z_{out} - z_{in})] \exp \left[-\frac{j k (x^2 + y^2)}{2 f} \right] \exp \left[-\frac{j k (x^2 + y^2)(z_{out} - z_{lens})}{2 (z_{out} - z_{lens})^2} \right] \times A \left(x, y, z_{in} \right) \exp \left[j k \frac{x^2}{2 f} \right] \exp \left[j k \frac{y^2}{2 f} \right] dx dy \quad [\text{II-14}]$$

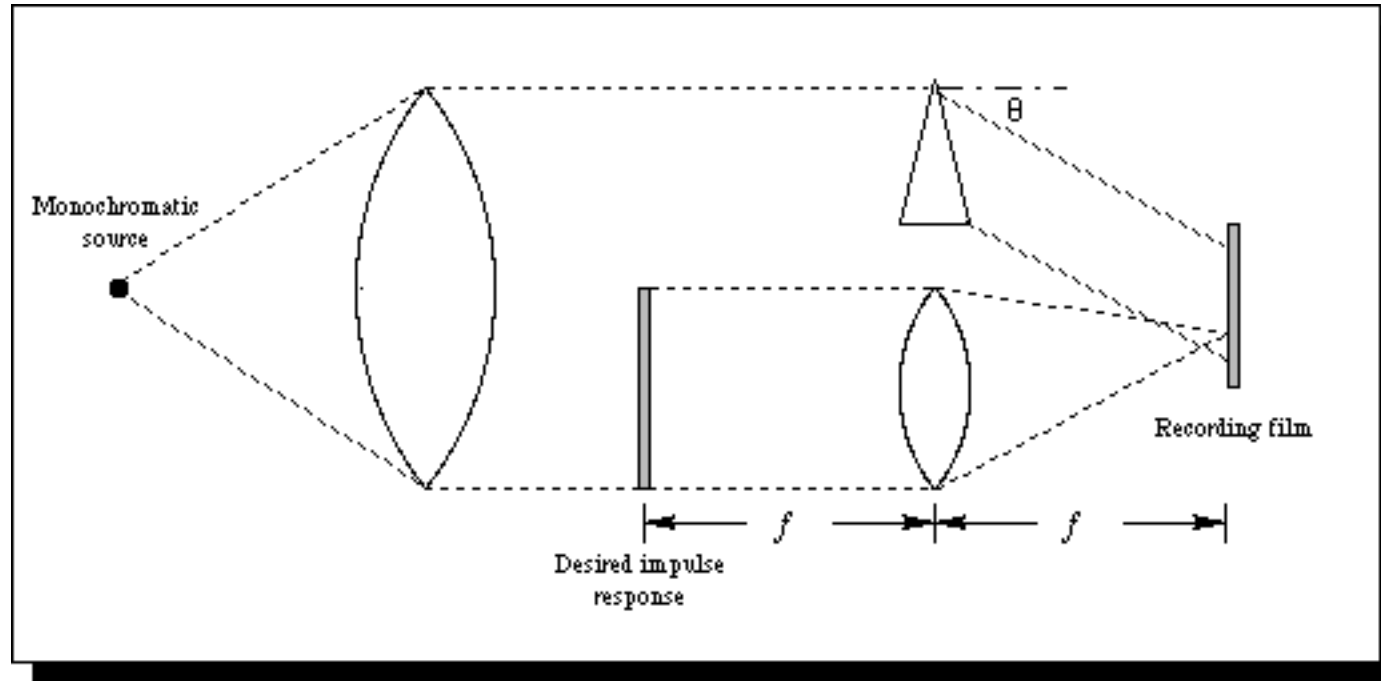
$$\text{If } A(k_x, k_y) = \left\{ A(x, y, z_{in}) \exp[jx k_x] \exp[jy k_y] \right\} dx dy \quad [\text{II-15}]$$

where $k_x = k(x/f)$ and $k_y = k(y/f)$,

$$A(x, y, z_{out}) = \frac{1}{j f} \exp[-j k (n D + z_{out} - z_{in})] \exp\left[-\frac{j k (x^2 + y^2)}{2 f} \left(1 - \frac{z_{lens} - z_{in}}{f}\right)\right] A(k_x, k_y) \quad [\text{II-16}]$$

SPATIAL FILTERING:

Let us first consider one method for generating **frequency plane masks**.



Modified Mach-Zehnder recording system for generating frequency-plane masks for a Vander Lugt filter

We suppose have some light distribution $g(x, y)$ of interest in the front focal-plane of a thin lens, then Equation [II-16] shows that the distribution in the back focal-plane is proportional to $G\left(\frac{kx}{f}, \frac{ky}{f}\right)$. To "bias" the final processed image, add to this distribution a **reference field** given by $R_0 \exp(jkx) \exp(-jkz)$ where $k = k \sin \theta$ (see figure above). The intensity due to these two fields is then proportional to

$$\begin{aligned} & \left| R_0 \exp(jkx) \exp(-jkz_{out}) + \frac{1}{j} \frac{1}{f} \exp[-jk(nD + 2f)] G\left(\frac{kx}{f}, \frac{ky}{f}\right) \right|^2 \\ & = |R|^2 + \frac{1}{f^2} \left| G\left(\frac{kx}{f}, \frac{ky}{f}\right) \right|^2 + \frac{R}{f} G\left(\frac{kx}{f}, \frac{ky}{f}\right) \exp(-jkx) + cc \end{aligned} \quad [\text{II-17}]$$

where all extraneous phase factors are absorbed into R . If we arrange the exposure and developing process so that the amplitude transmittance of the film is proportional to the intensity -- *i.e.* the over all contrast ≈ 1 (see the **Hurter-Driffield curve** at the end of this section) that resultant transparency is given by

$$t(x, y) = |R|^2 + \frac{1}{f^2} \left| G\left(\frac{kx}{f}, \frac{ky}{f}\right) \right|^2 + \frac{R}{f} G\left(\frac{kx}{f}, \frac{ky}{f}\right) \exp(-jkx) + cc. \quad [\text{II-18}]$$

If the developed transparency or filter is placed in the **frequency-plane** of a classic coherent optical processing system -- *i.e.* to identical thin lenses separated by a distance $2f$ -- and a **transparency to be tested** (distribution $f(x, y)$) is placed in the **input-plane** -- *i.e.* a distance in front of one lens -- the field distribution just to the right of the frequency-plane, when both transparencies are illuminated with coherent light, is given by

$$A(x, y, z_{freq}^+) = \frac{|R|^2}{(f)^2} F\left(\frac{k_x}{f}, \frac{k_y}{f}\right) + \frac{1}{(f)^3} \left| G\left(\frac{k_x}{f}, \frac{k_y}{f}\right) \right|^2 F\left(\frac{k_x}{f}, \frac{k_y}{f}\right) + \frac{R}{(f)^2} G\left(\frac{k_x}{f}, \frac{k_y}{f}\right) F\left(\frac{k_x}{f}, \frac{k_y}{f}\right) \exp(-j k_x x) + \frac{R}{(f)^2} G\left(\frac{k_x}{f}, \frac{k_y}{f}\right) F\left(\frac{k_x}{f}, \frac{k_y}{f}\right) \exp(+j k_x x) \quad \text{[II-19]}$$

where again extraneous phase factors have been suppressed. The transformation to the output plane of the third and fourth terms yield

$$A^{(3)}(x, y, z_{out}) = \frac{R}{f} \frac{1}{2} \int G(k_x, k_y) F(k_x, k_y) \exp[j k_x x - \frac{f}{k} \exp[j k_y y]] dk_x dk_y \quad \text{[II-20]}$$

$$A^{(4)}(x, y, z_{out}) = \frac{R}{f} \frac{1}{2} \int G(k_x, k_y) F(k_x, k_y) \exp[j k_x x + \frac{f}{k} \exp[j k_y y]] dk_x dk_y \quad \text{[II-21]}$$

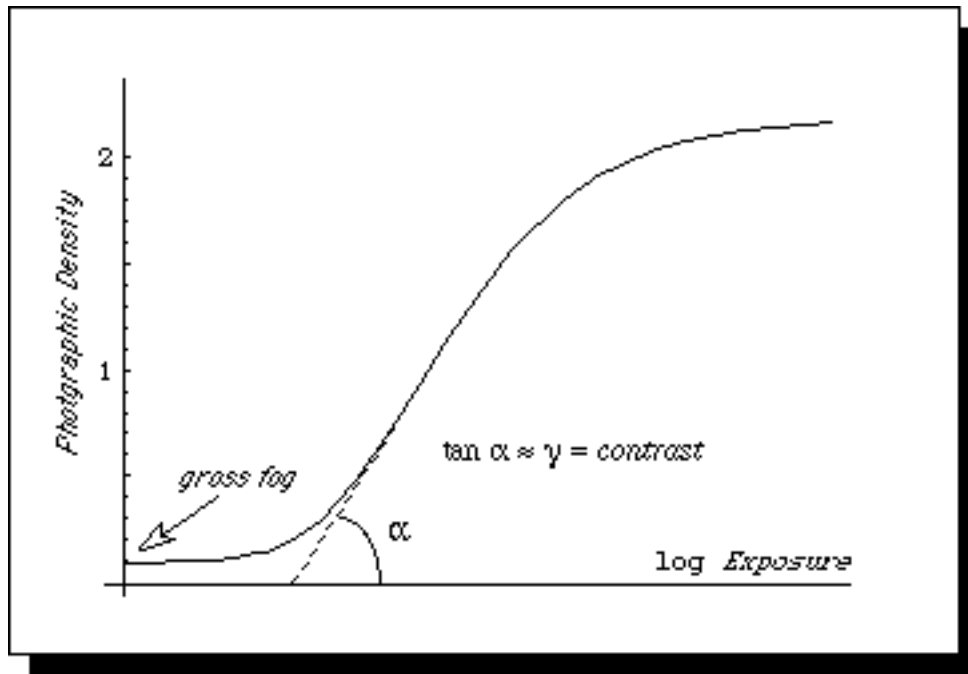
Using the definition in Equation [II-15] we see that

$$A^{(3)}(x, y, z_{out}) = \frac{R}{f} \int g(x, y) f\left(x - x - \frac{f}{k}, y - y\right) dx dy_1 \quad \text{[II-22]}$$

is the **convolution** of the two function g and f and

$$A^{(4)}(x, y, z_{out}) = \frac{R}{f} \int g(x_1, y_1) f\left(x + x_1 + \frac{f}{k}, y + y_1\right) dx_1 dy_1 \quad \text{[II-23]}$$

is their **cross-correlation**.



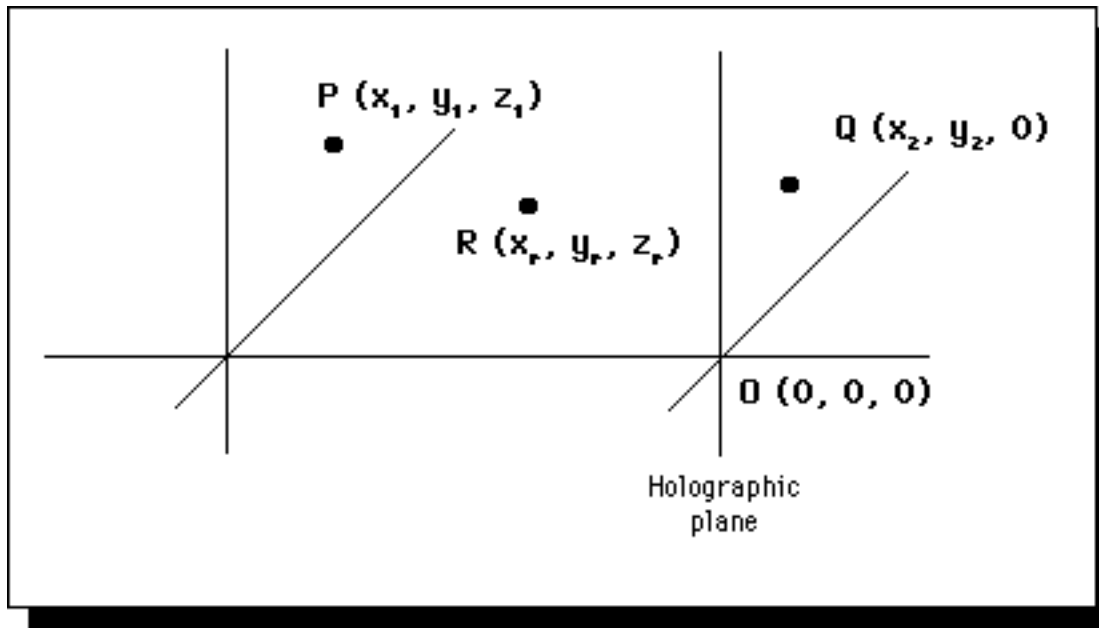
The Hurter-Driffield Curve (1890)

Characterizes the functional relationship between *photographic density* which is equal to the logarithm of the inverse of the *intensity transmittance* of a developed transparency and *exposure* which is the product of the incident *intensity* and the duration of the exposure.

III. IMAGING PROPERTIES OF HOLOGRAPHY:

One of the most important applications of holography is in the construction of beam forming or imaging devices. To study the imaging properties of holograms, we make the following reasonable, but simplifying assumption:

1. The sources of all fields -- *reference, subject, and playback* -- are point sources.
2. Recording medium is thin and has a quadratic response.
3. Fields may be treated in the paraxial approximation.



From the subject point source at P we assume a field

$$U_P(\vec{r}, z) = C_P \frac{\exp[-j k_r |\vec{r} - \vec{r}_P|]}{|\vec{r} - \vec{r}_P|} = |C_P| \exp(-j \phi_P) \quad [\text{III-1}]$$

and from the reference point source at R we assume a field

$$U_R(\vec{r}, z) = C_R \frac{\exp[-j k_r |\vec{r} - \vec{r}_R|]}{|\vec{r} - \vec{r}_R|} = |C_R| \exp(-j \phi_R) \quad [\text{III-2}]$$

The recorded signal in the holographic plane is proportional to

$$I(\vec{r}, z) = |U_R + U_P|^2 = |C_R|^2 + |C_P|^2 + 2 |C_R| |C_P| \cos(\phi_P - \phi_R) \quad [\text{III-3}]$$

For convenience, we express the phase of the signals at the point Q taking their phase at O as reference -- *i.e.*

$$\begin{aligned}
 p &= k_r (PQ - PO) \\
 &= k_r \left\{ \left[(x_2 - x_1)^2 + (y_2 - y_1)^2 + z_1^2 \right]^{1/2} - \left[x_1^2 + y_1^2 + z_1^2 \right]^{1/2} \right\} \\
 &= k_r z_1 \left[1 + \frac{(x_2 - x_1)^2 + (y_2 - y_1)^2}{z_1^2} \right]^{1/2} - \left[1 + \frac{x_1^2 + y_1^2}{z_1^2} \right]^{1/2}
 \end{aligned} \quad \text{[III-4]}$$

In the paraxial approximation

$$p \approx \frac{k_r}{2 z_1} (x_2^2 + y_2^2 - 2 x_2 x_1 - 2 y_2 y_1) \quad \text{[III-5]}$$

and similarly

$$r \approx \frac{k_r}{2 z_r} (x_2^2 + y_2^2 - 2 x_2 x_r - 2 y_2 y_r) . \quad \text{[III-6]}$$

Therefore, in the paraxial approximation

$$p - r \approx k_r (x_2^2 + y_2^2) \left[\frac{1}{2 z_1} - \frac{1}{2 z_r} \right] - x_2 \left[\frac{x_1}{z_1} - \frac{x_r}{z_r} \right] - y_2 \left[\frac{y_1}{z_1} - \frac{y_r}{z_r} \right] . \quad \text{[III-7]}$$

Examples of types of holograms:

1. **"On Axis" or Gabor Holograms:** ($x_1 = y_1 = x_r = y_r = 0$, $z_1 = -u$ and $z_r = -v$)

$$p - r \approx \frac{k_r}{2} (x_2^2 + y_2^2) \left[\frac{1}{v} - \frac{1}{u} \right] = \frac{x_2^2 + y_2^2}{2 f} . \quad \text{[III-8]}$$

The condition

$$r_p - r_r = n \lambda \quad \text{or} \quad x_2^2 + y_2^2 = n \lambda z_r \quad \text{[III-9]}$$

defines the points on circles of constructive interference or maximum film darkening ("Fresnel" zone plate)

2. **"Off Axis" or Leith-Upatnicks Holograms:** ($x_1 = y_1 = x_r = y_r = 0$, $z_1 = -u$ and $z_r = -v$)

The points of constructive interference or maximum film darkening lie on circles ("off-centered" zone plates) centered at

$$(x_2, y_2) = \left(\frac{x_r z_1 - x_1 z_r}{z_1 - z_r}, \frac{y_r z_1 - y_1 z_r}{z_1 - z_r} \right) \quad \text{[III-10a]}$$

with radius

$$\frac{x_r z_1 - x_1 z_r}{z_1 - z_r}^2 + \frac{y_r z_1 - y_1 z_r}{z_1 - z_r}^2 + n \lambda \frac{z_1 z_r}{z_1 - z_r} \quad \text{[III-10b]}$$

RECONSTRUCTION OR PLAYBACK PROCESS

From the playback point source at C we assume a field

$$E_{PB}(\vec{r}, z) = C_{PB} \frac{\exp[-j k_{pb} |\vec{r} - \vec{r}_{PB}|]}{|\vec{r} - \vec{r}_{PB}|} = |E_{PB}| \exp(-j k_{pb} z) \quad \text{[III-11]}$$

where we allow for the possibility of using a different wavelength in the playback process. That process yields, among other things, a **"virtual" signal**

$$E_{PB}(\vec{r}, z) = |E_{PB}| \exp(-j k_{real} z) \quad \text{[III-12]}$$

where $z_{virtual} = z_{PB} + z_R - z_P$ and a "real" signal

$$U_{PB, R, P} = |U_{PB}| |U_R| |U_P| \exp(-j z_{real}) \quad [\text{III-13}]$$

where $z_{real} = z_{PB} - z_R + z_P$. The hologram may be photographically scaling (enlarged or reduced) by a factor m $x_2/x_1 = y_2/y_1$. If so the phase of the regenerated signals may be expressed as

$$\begin{aligned} U_{virtual, real} &= k_{pb} \frac{1}{2 z_{pb}} (x_2^2 + y_2^2 - 2 x_2 x_{pb} - 2 y_2 y_{pb}) \\ &\mp k_r \frac{1}{2 z_r} (x_2^2 + y_2^2 - 2 x_2 x_r - 2 y_2 y_r) \\ &\pm k_r \frac{1}{2 z_1} (x_2^2 + y_2^2 - 2 x_2 x_1 - 2 y_2 y_1) \end{aligned} \quad [\text{III-14a}]$$

or as

$$\begin{aligned} U_{virtual, real} &= k_{pb} \frac{1}{2} (x_2^2 + y_2^2) \frac{1}{z_{pb}} \pm \frac{\mu}{m^2 z_1} \mp \frac{\mu}{m^2 z_r} \\ &- 2 x_2 \frac{x_{pb}}{z_{pb}} \pm \frac{\mu x_1}{m z_1} \mp \frac{\mu x_r}{m z_r} - 2 y_2 \frac{y_{pb}}{z_{pb}} \pm \frac{\mu y_1}{m z_1} \mp \frac{\mu y_r}{m z_r} \end{aligned} \quad [\text{III-14b}]$$

where $\mu = k_r/k_{pb} = z_{pb}/z_r$. If the holographic process is to "image" a point source, the point image must have over the holographic plane the relative phase

$$\frac{k_{pb}}{2 z_3} (x_2^2 + y_2^2 - 2 x_2 x_3 - 2 y_2 y_3) \quad [\text{III-15}]$$

so that

$$\frac{1}{z_3 \begin{smallmatrix} \text{virtual} \\ \text{real} \end{smallmatrix}} = \frac{1}{z_{pb}} \pm \frac{\mu}{m^2} \frac{1}{z_1} \mp \frac{\mu}{m^2} \frac{1}{z_r} \quad [\text{III-16a}]$$

$$x_3 \begin{smallmatrix} \text{virtual} \\ \text{real} \end{smallmatrix} = m \frac{m z_1 z_{pb} z_r \pm \mu z_{pb} z_r x_1 \mp \mu z_{pb} z_1 x_r}{m^2 z_1 z_r \pm \mu z_{pb} z_r \mp \mu z_{pb} z_1} \quad [\text{III-16b}]$$

$$y_3 \begin{smallmatrix} \text{virtual} \\ \text{real} \end{smallmatrix} = m \frac{m z_1 z_{pb} z_r \pm \mu z_{pb} z_r y_1 \mp \mu z_{pb} z_1 y_r}{m^2 z_1 z_r \pm \mu z_{pb} z_r \mp \mu z_{pb} z_1} . \quad [\text{III-16c}]$$

and, therefore, the lateral image magnification is given by

$$\frac{x_3 \begin{smallmatrix} \text{virtual} \\ \text{real} \end{smallmatrix}}{x_1} = \frac{y_3 \begin{smallmatrix} \text{virtual} \\ \text{real} \end{smallmatrix}}{y_1} = \pm \frac{\mu}{m} \frac{z_3 \begin{smallmatrix} \text{virtual} \\ \text{real} \end{smallmatrix}}{z_1} \quad [\text{III-17}]$$

APPENDIX

THE PARAXIAL WAVE EQUATION

We derive here the paraxial approximation of the Helmholtz equation. To that end, we start with the homogeneous Helmholtz equation for the electric field in the form

$$[\text{div grad}] \vec{\mathbf{E}}(\vec{\mathbf{r}}, z) + k^2 \vec{\mathbf{E}}(\vec{\mathbf{r}}, z) = \nabla^2 \vec{\mathbf{E}}(\vec{\mathbf{r}}, z) + k^2 \vec{\mathbf{E}}(\vec{\mathbf{r}}, z) = 0 \quad [\text{A-1}]$$

where $k^2 = \omega^2 \mu(\omega)$. The "searchlight" mode of propagation that we seek is an elaboration of a plane wave propagating in, say, the z -direction, and we assume that a particular component of that field may be written in the form

$$\mathbf{E}(\vec{\mathbf{r}}, z) = \mathbf{E}_0(\vec{\mathbf{r}}) \exp(-jkz) \quad [\text{A-2}]$$

where the function $\mathbf{E}_0(\vec{\mathbf{r}})$ represents a spatial modulation or "masking" of the plane wave. The z -direction is obviously special and it is, therefore, useful -- nay, essential -- to appropriately parse the spatial differential operators. For the **grad** operator we may write

$$\text{grad} \{ \text{anything} \} = \nabla_{\text{tr}} \{ \text{anything} \} + \hat{\mathbf{z}} \frac{\partial}{\partial z} \{ \text{anything} \} \quad [\text{A-3}]$$

where the transverse **grad** operator is given by, for example,

$$\nabla_{\text{tr}} \{ \text{anything} \} = \hat{\mathbf{x}} \frac{\partial}{\partial x} \{ \text{anything} \} + \hat{\mathbf{y}} \frac{\partial}{\partial y} \{ \text{anything} \} . \quad [\text{A-4}]$$

Thus, this **grad** operator acting on field component represented in Equation [A-2] may be parsed as

$$\nabla \mathbf{E}(\vec{\mathbf{r}}, z) = \nabla_{\text{tr}} \mathbf{E}_0(\vec{\mathbf{r}}) + \hat{\mathbf{z}} \frac{\partial}{\partial z} \mathbf{E}_0(\vec{\mathbf{r}}) - jk \mathbf{E}_0(\vec{\mathbf{r}}) \exp(-jkz) \quad [\text{A-5}]$$

and the **Laplacian** operator acting on field component represented in Equation [A-2] may be parsed as

$$\begin{aligned} \nabla^2 \mathbf{E}(\vec{\mathbf{r}}, z) &= \nabla_{\text{tr}}^2 \mathbf{E}(\vec{\mathbf{r}}, z) \\ &= \nabla_{\text{tr}}^2 + \hat{\mathbf{z}} \frac{\partial^2}{\partial z^2} \mathbf{E}(\vec{\mathbf{r}}, z) + \hat{\mathbf{z}} \frac{\partial}{\partial z} \mathbf{E}(\vec{\mathbf{r}}, z) - j k \mathbf{E}(\vec{\mathbf{r}}, z) \exp(-j k z) \quad [\text{A-6}] \\ &= \nabla_{\text{tr}}^2 \mathbf{E}(\vec{\mathbf{r}}, z) + \frac{\partial^2}{\partial z^2} \mathbf{E}(\vec{\mathbf{r}}, z) - j 2k \frac{\partial}{\partial z} \mathbf{E}(\vec{\mathbf{r}}, z) - k^2 \mathbf{E}(\vec{\mathbf{r}}, z) \exp(-j k z) \end{aligned}$$

where the transverse **Laplacian** operator is given by, for example,

$$\nabla_{\text{tr}}^2 \{ \text{anything} \} = \frac{\partial^2}{\partial x^2} \{ \text{anything} \} + \frac{\partial^2}{\partial y^2} \{ \text{anything} \} \quad [\text{A-7}]$$

Therefore, the parsed Helmholtz equation (**without approximation**) becomes

$$\nabla_{\text{tr}}^2 \mathbf{E}(\vec{\mathbf{r}}, z) + \frac{\partial^2}{\partial z^2} \mathbf{E}(\vec{\mathbf{r}}, z) - j 2k \frac{\partial}{\partial z} \mathbf{E}(\vec{\mathbf{r}}, z) = 0. \quad [\text{A-8}]$$

The **paraxial approximation** is precisely defined by the condition

$$\frac{\partial^2}{\partial z^2} \mathbf{E}(\vec{\mathbf{r}}, z) \ll 2k \frac{\partial}{\partial z} \mathbf{E}(\vec{\mathbf{r}}, z) \quad [\text{A-9}]$$

which means that the longitudinal variation in the derivative of the modulation function, $\frac{\partial}{\partial z} \mathbf{E}(\vec{\mathbf{r}}, z)$, changes very little in a distance comparable to the nominal wavelength of the beam -- *i.e.* $2/k$. In this approximation, we neglect the second term of Equation [A-8] to obtain the equation

$$\nabla_{\vec{r}}^2 (\vec{r}, z) - j 2k \frac{\partial}{\partial z} (\vec{r}, z) = 0$$

[A-10]

which is called the **paraxial approximation** of the wave equation.⁵

⁵ This is also the form of the famous Schrödinger equation used in quantum mechanics. In the Schrödinger equation the first order derivative is a time derivative (*i.e.* $\frac{\partial}{\partial t}$), the Laplacian is a full 3D Laplacian (*i.e.* $\nabla_{\{x, y, z\}}^2$) and field is a particle field.